

Multiscale modelling of dislocation patterning

Péter Dusán Ispánovity¹, Stefanos Papanikolaou², István
Groma¹

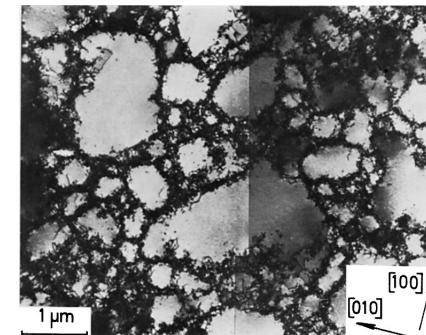
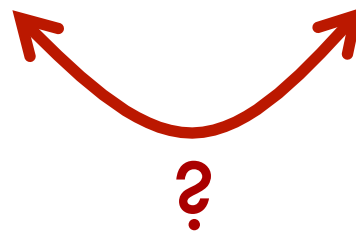
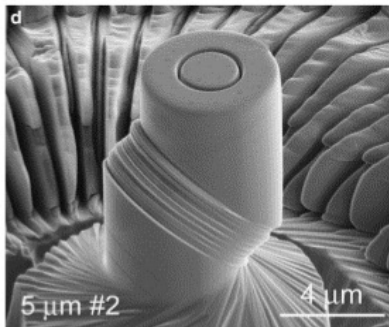
¹ Eötvös University Budapest

² West Virginia University

Motivation

- Crystal plasticity is undoubtedly a critical phenomenon
 - Power-law distributions, scaling laws
 - Details unclear
- Complex system far from equilibrium

- Dislocations tend to form patterns
 - Various patterns under different conditions
 - Details unclear
- Complex system far from equilibrium



Outline

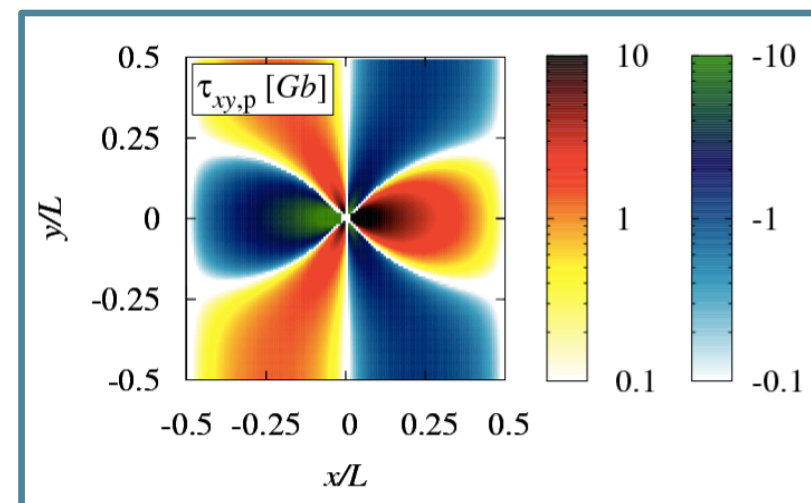
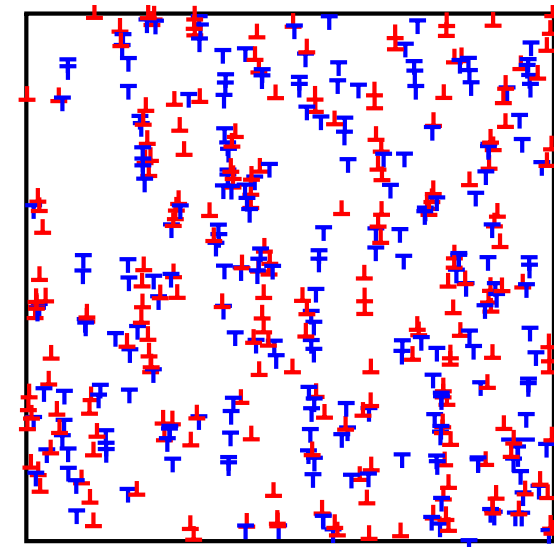
- Properties of 2D dislocation systems
 - Avalanche distributions – extended criticality
 - Formation of dipolar walls
- Continuum modelling
 - Stochastic modelling
 - Deterministic continuum models
- 2D stochastic continuum framework
 - Evolution equations – backstress, flow stress
 - Dipolar wall formation
 - Comparison with DDD
- Summary

2D dislocation model

2D DDD

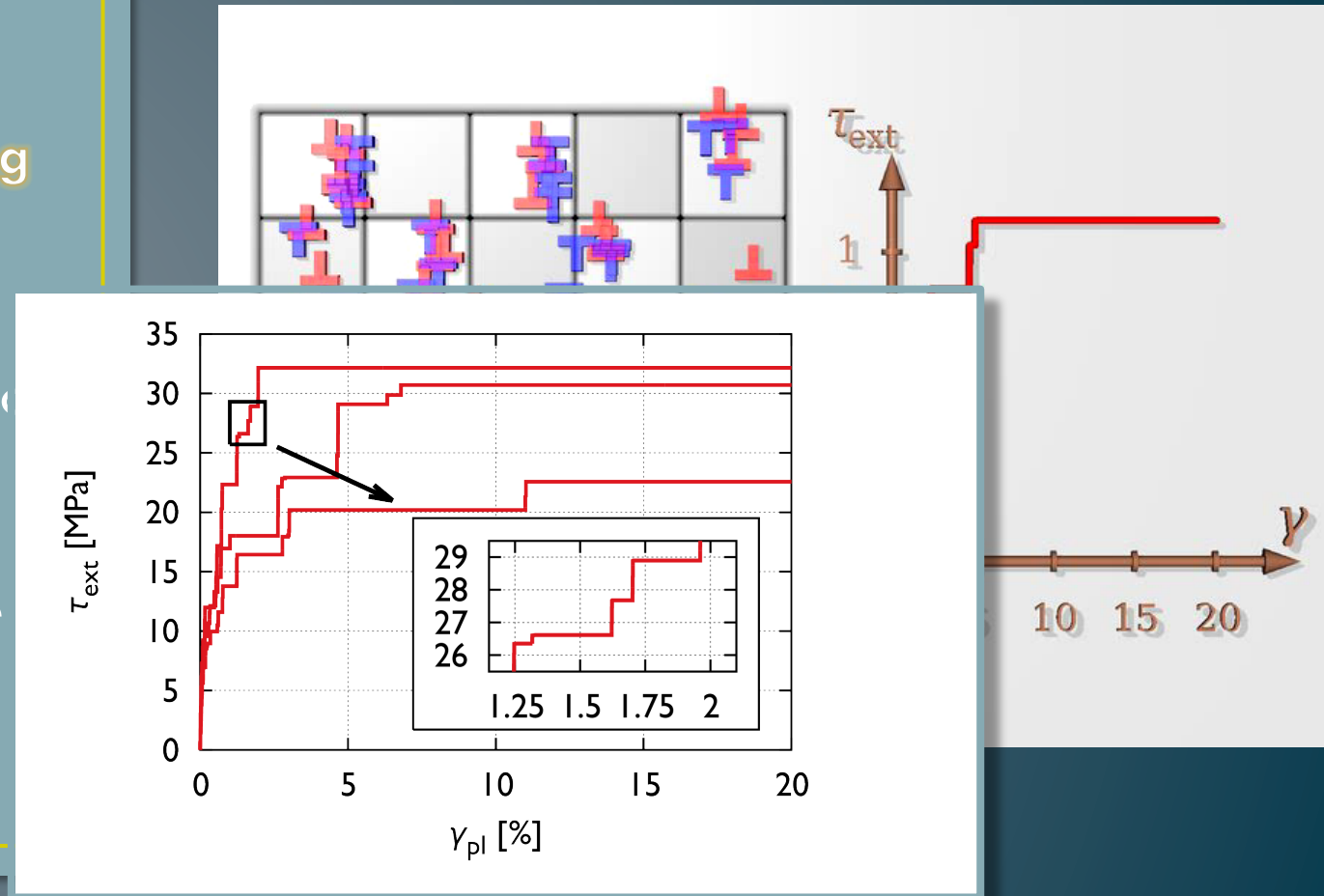
- Parallel edge dislocations in single slip
- Periodic boundary conditions
- Number of dislocations: N
- Sign of dislocations: $s_i = \pm 1$
- Stress-field of an individual dislocation: σ_{xy}
- Overdamped motion:

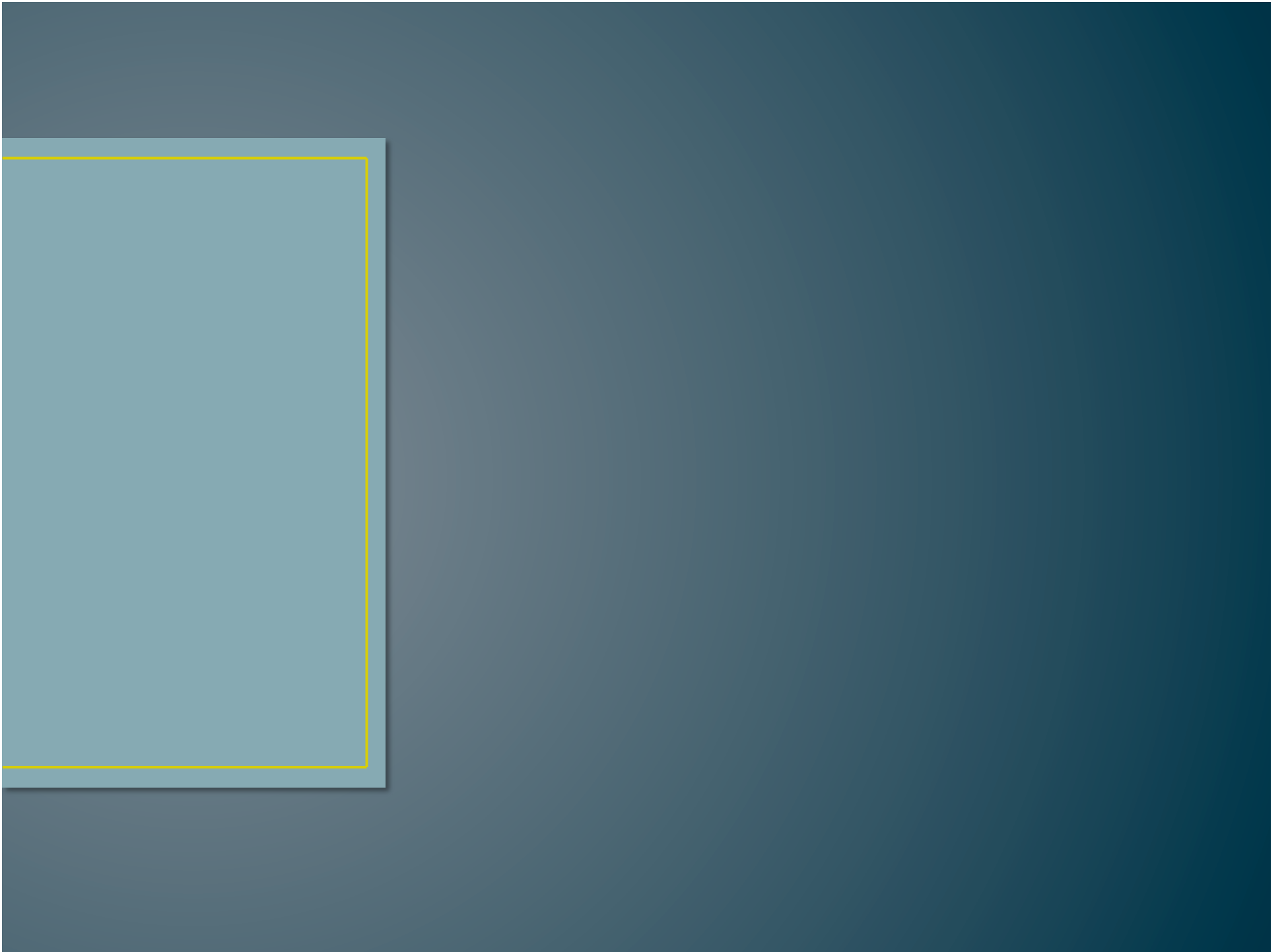
$$\dot{x}_i = s_i \left[\sigma_{\text{ext}} + \sum_{j=1}^N s_j \sigma_{xy}(\mathbf{r}_i - \mathbf{r}_j) \right]$$



Plastic shearing in 2D

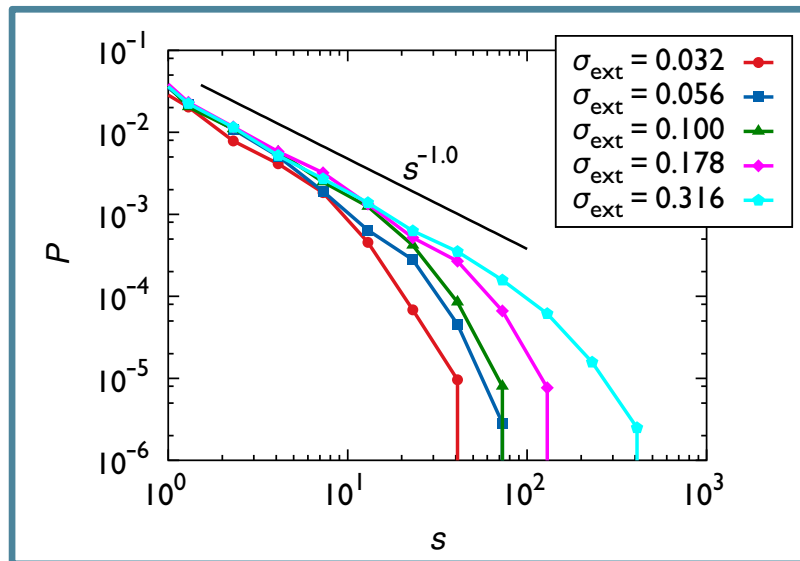
- Initial relaxation step
- Quasi-static stress increase



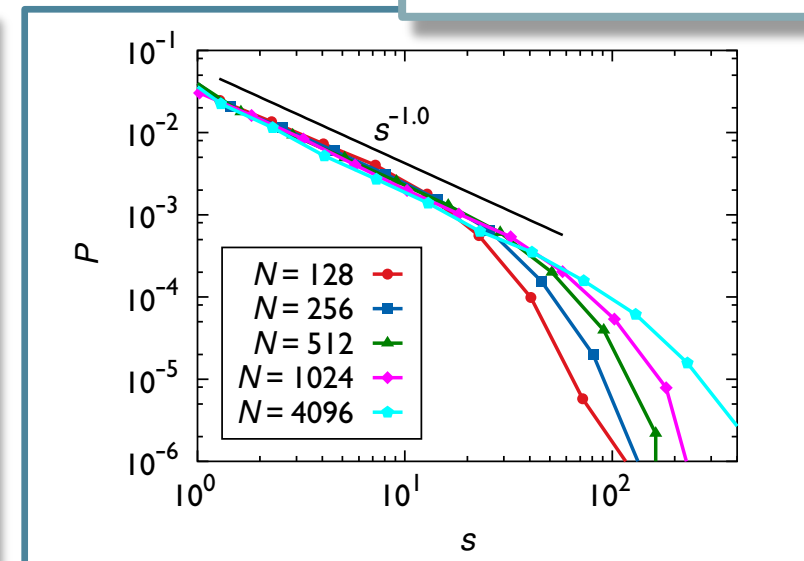


Strain burst distributions

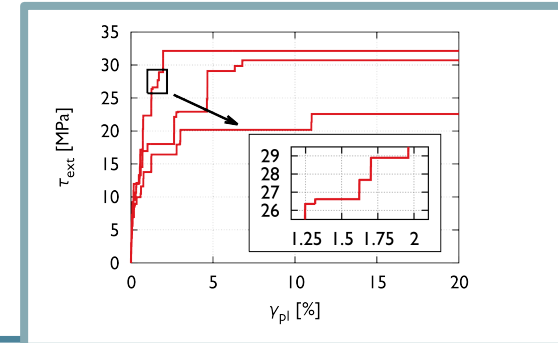
- Avalanche size s is the total area swept
- System size: $L = \sqrt{N}$



Dependence on the applied stress ($N = 4096$)

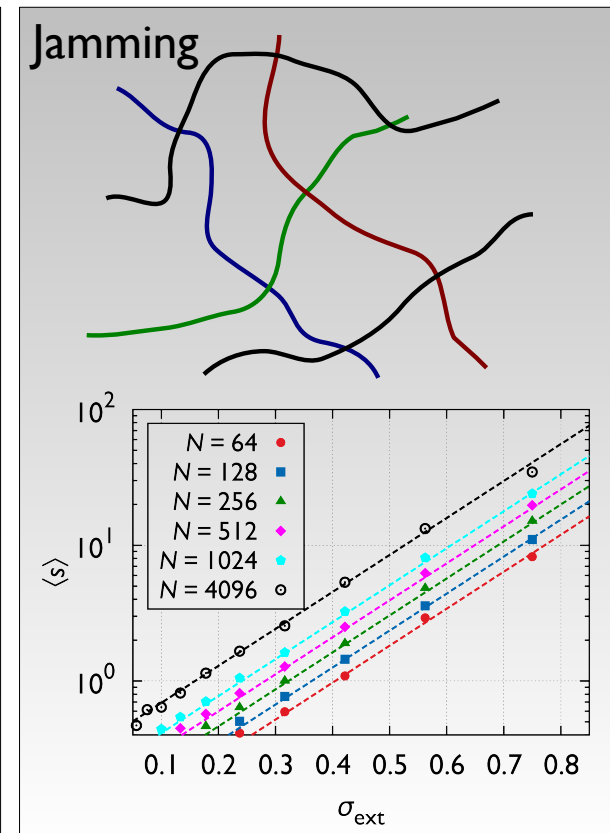
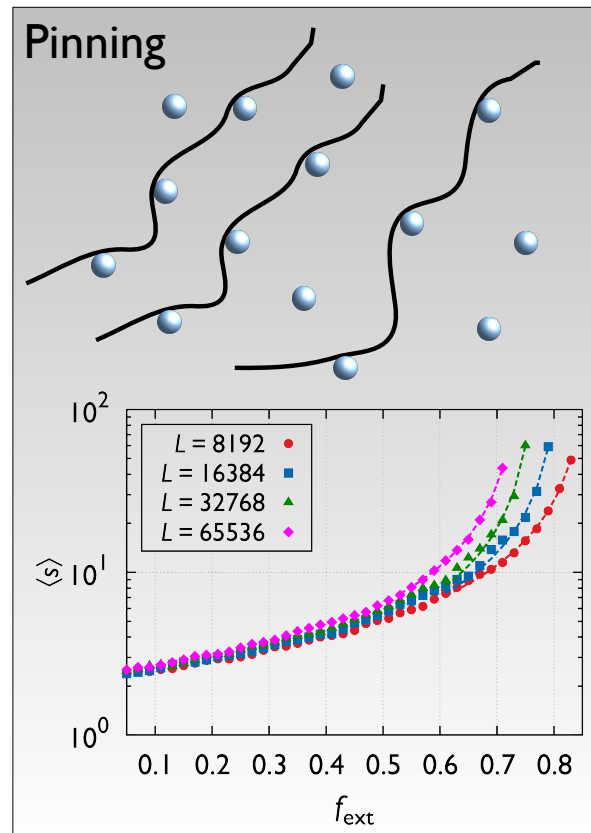


Dependence on the system size ($\sigma_{\text{ext}} = 0.316$)



Extended criticality

- The system is always critical
 - Other indications (relaxation, system size scaling, pseudo gap)
 - Avalanches always span the whole system
 - Also true in 3D



PD Ispánovity, L Laurson, M Zaiser, I Groma, S Zapperi, M Alava, PRL, 2014

A Lehtinen, G Costantini, M Alava, S Zapperi, L Laurson, PRB, 2016

M Ovaska, A Lehtinen, M Alava, L Laurson, S Zapperi, PRL, 2017

Conclusions of 2D results

Disadvantages

- Toy model
- No multiple slip
- No short-range interactions
- No curvature

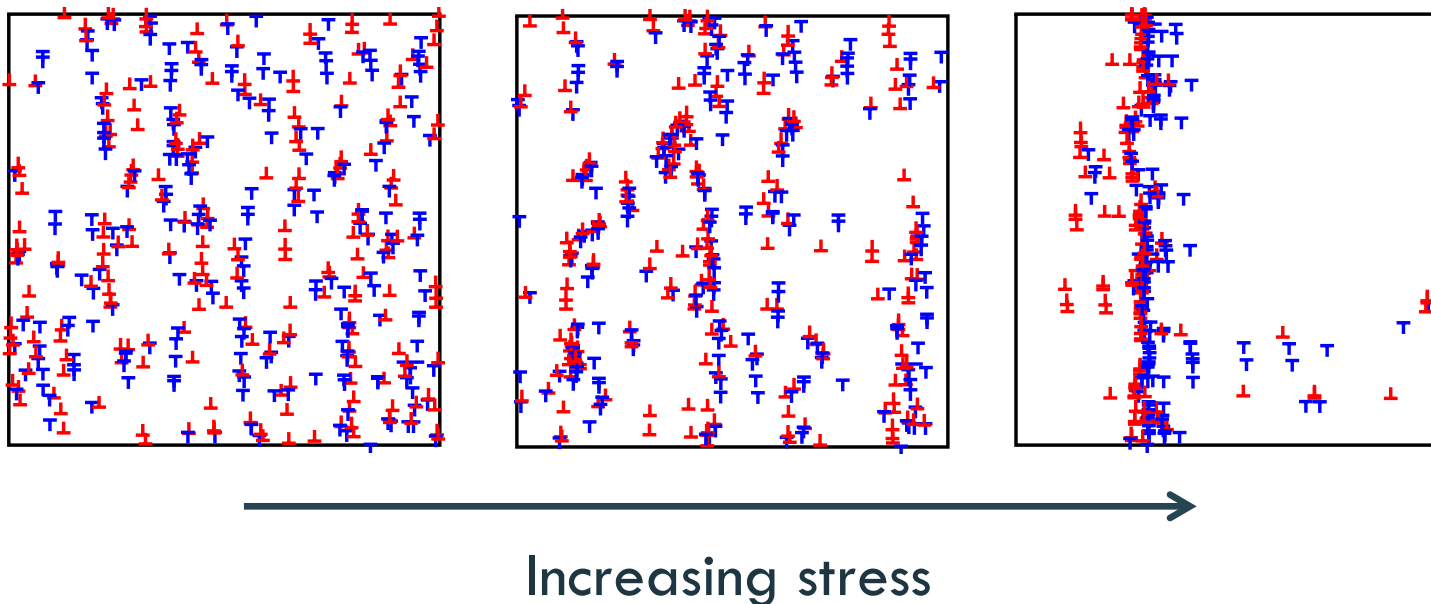
Advantages

- Toy model
 - Numerically feasible
 - Theoretically feasible

- The 2D system is a limiting case theoretical models should be capable of describing
- It is ideal for developing concepts and methods for describing and understanding collective phenomena

Pattern evolution in 2D DDD

- With increasing stress dipolar walls form
- These are the ‘strongest’ objects in 2D single slip

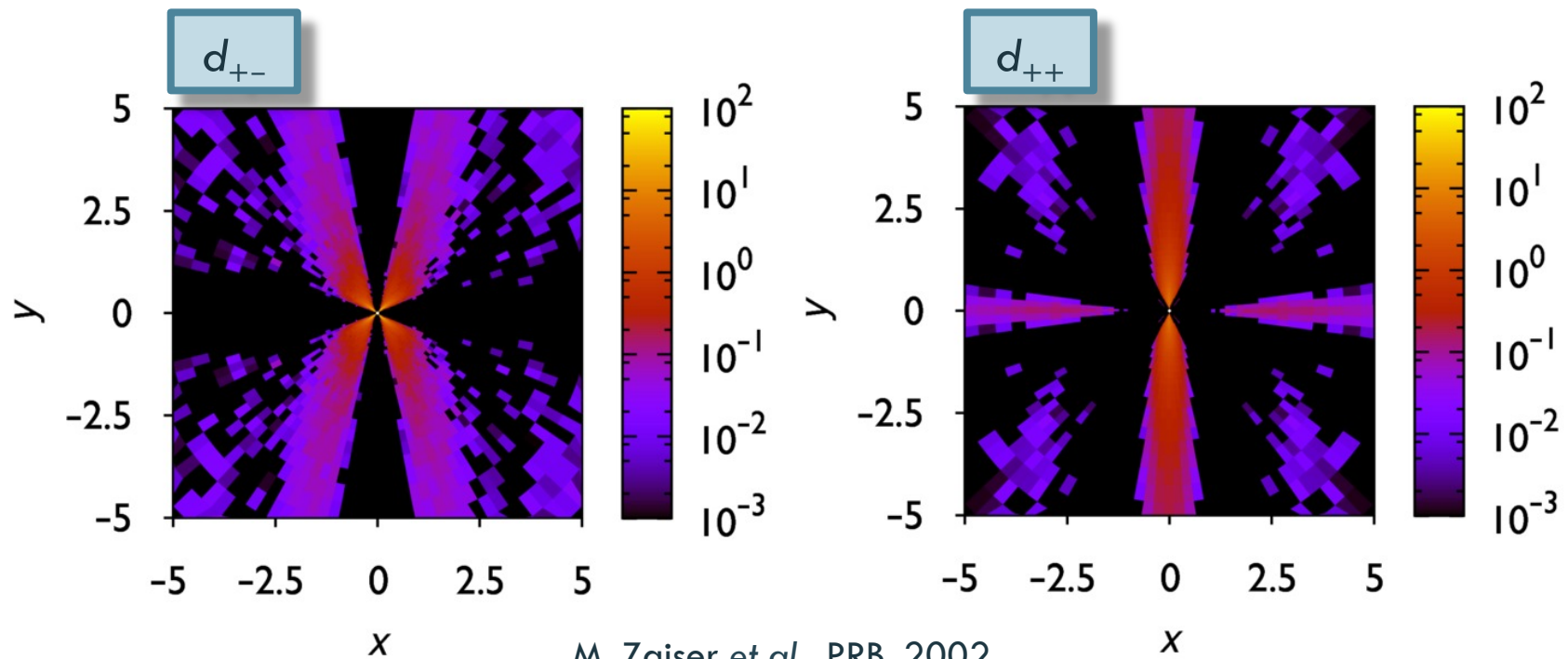


C Zhou, C Reichardt, CJO Reichardt, IJ Beyerlein, Sci Rep, 2015

P Szabó, PD Ispánovity, I Groma, PRB, 2015

Spatial correlation functions

- Correlation functions: dislocation density around a randomly chosen positive sign dislocation
 - d_{+-} : relative density of the negative sign dislocations
 - d_{++} : relative density of the positive sign dislocations



Continuum modelling of dislocations

Stochastic elastoplastic models

- Aim: modelling strain bursts
 - Local yield threshold distributions

Continuum dislocation dynamics

- Aim: modelling local strain evolution and patterns
- Local dislocation density fields
 - Deterministic

Stochastic plasticity models

2D continuum equations



Assuming $\rho = \text{const.}$

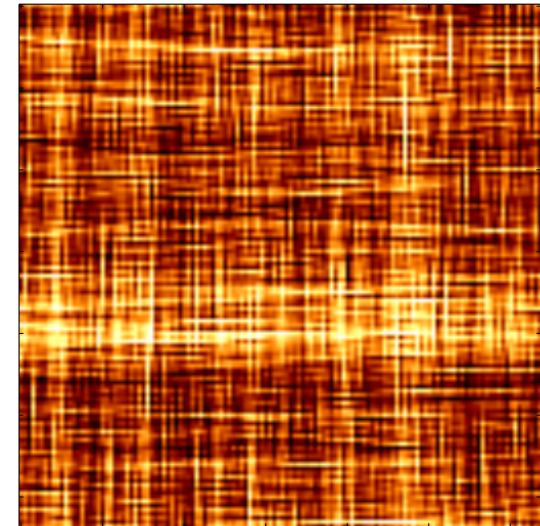
Evolution equation for plastic strain

$$\dot{\gamma} = \rho b M_0 (\tau_{mf} - \tau_f)$$



Considering τ_f as a
stochastic variable

Stochastic CA model for plasticity



Strain pattern upon
shear

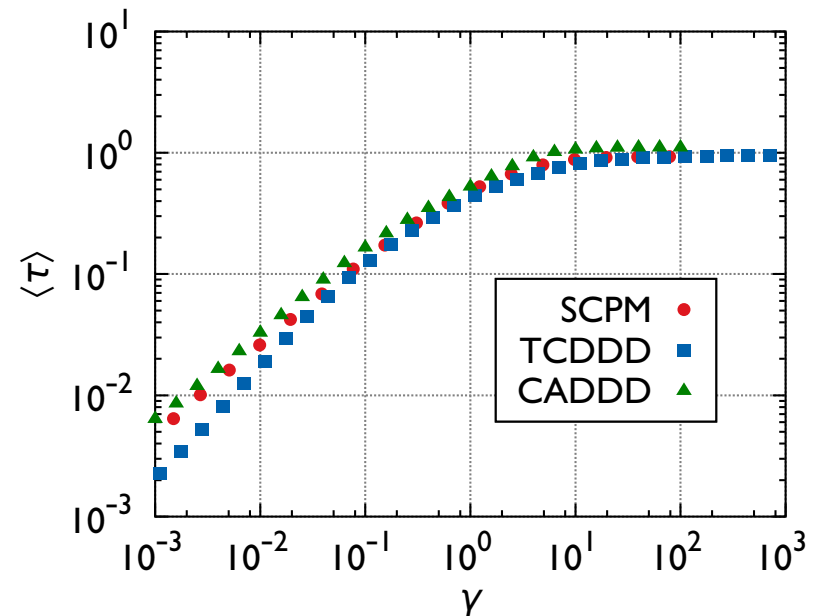
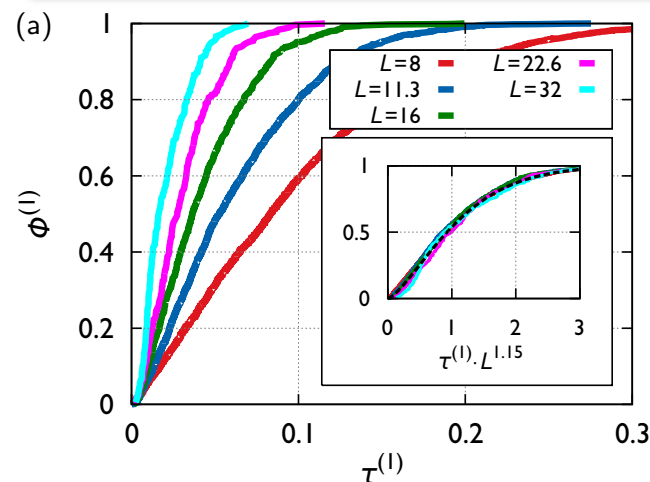
M Zaiser, P Moretti, J Stat Mech, 2005
S Sandfeld et al, J Stat Mech, 2015

Setting the yield threshold distribution

The distribution of the stress at the first strain burst

- Shape parameter: $\beta = 1.4$

Cumulative distribution of $\tau^{(1)}$

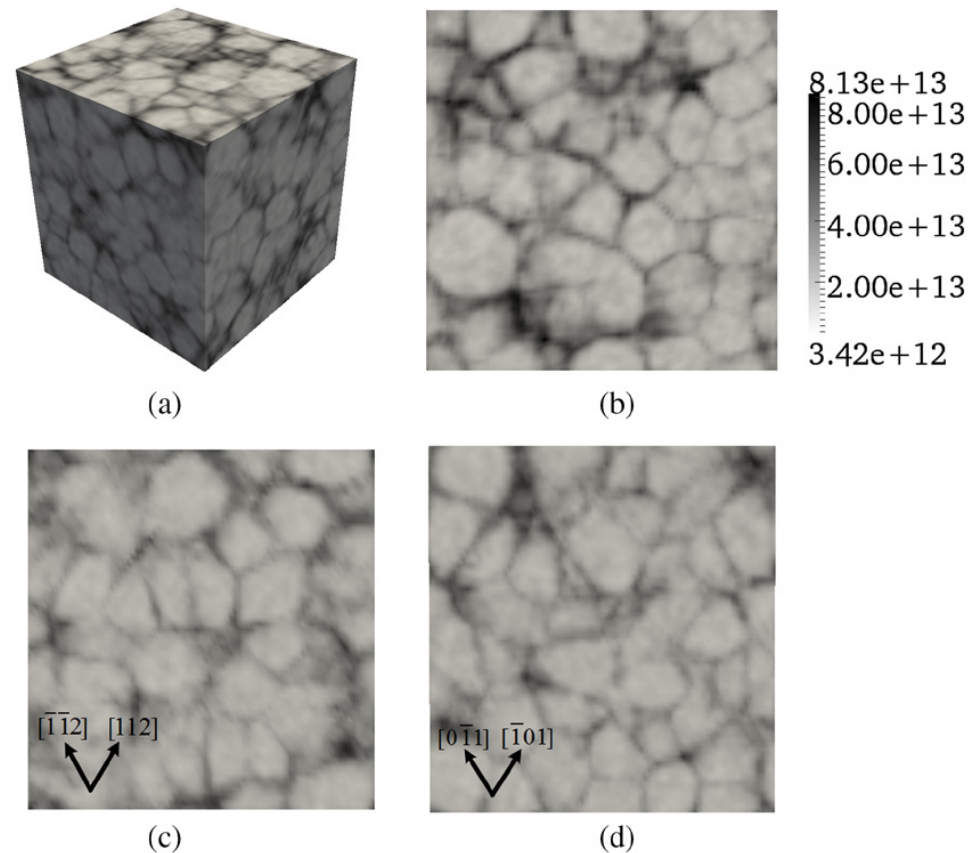


$$\Phi^{(1)}(\tau^{(1)}) = 1 - \exp\left(-\frac{1}{M} \left(\frac{\tau^{(1)}}{\tau_0}\right)^\beta\right)$$

PD Ispánovity, D Tüzes, P Szabó, M Zaiser,
I Groma, PRB, 2017

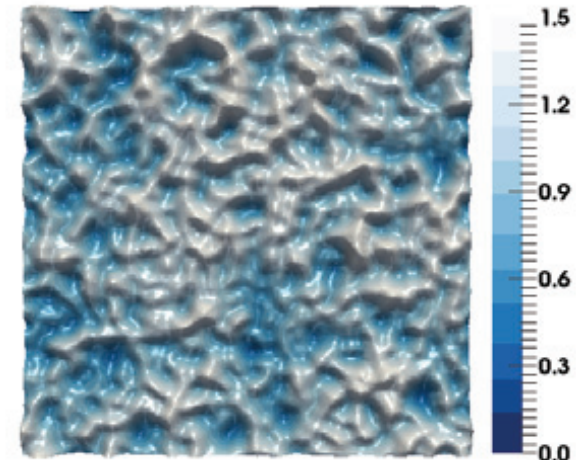
Continuum modelling of cell structures I.

- Mean-field 3D continuum dislocation dynamics model
- Enabling cross-slip leads to the formation of a cell structure

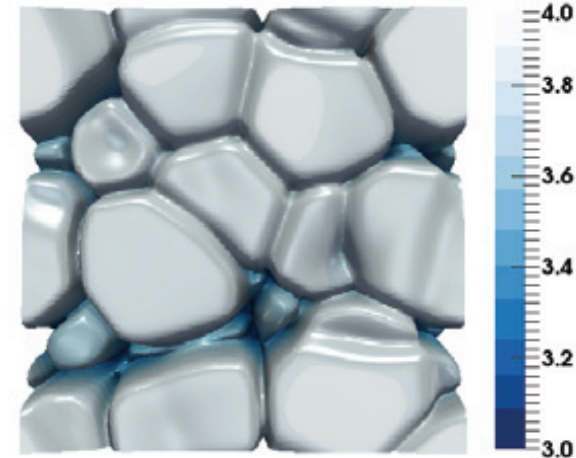


Continuum modelling of cell structures II.

- CDD model of Hochrainer and co-workers
- Neglecting elastic stress interactions and keeping a Taylor-like friction stress leads to a cellular pattern



Initial

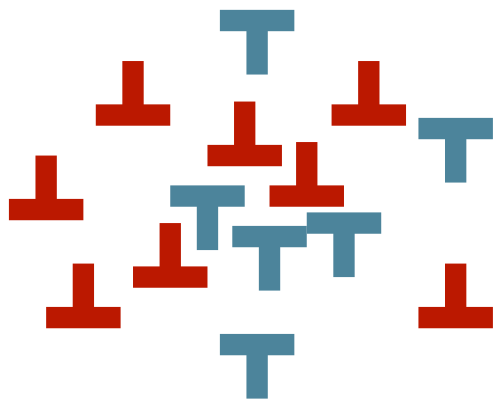


Stationary

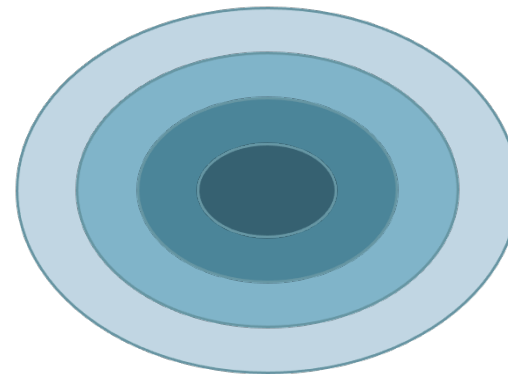
S Sandfeld, M Zaiser, Mod Simul Mater Sci Eng, 2015

Objectives

- Multiscale modelling of dislocation patterning
 - Quantitative comparison of *discrete* and *continuum* models
 - Validation of the continuum model, e.g. back-stress
 - Systematic determination of the fitting parameters of the continuum model
 - Simplest case: 2D single slip



Discrete representation



Continuum representation

Continuum models

- Evolution equations of dislocation densities

$$\partial_t \rho_i + \nabla \cdot \mathbf{j}_i = f_{\text{reaction}}(\rho_i, \tau_{\text{ext}}, \dots)$$

- ρ_i : some scalar dislocation density field
 - \mathbf{j}_i : flux of the given density
 - f_{reaction} : multiplication, annihilation, cross-slip, etc.
-
- Question:
 - What scalar densities to use?
 - What is the reaction term?
 - How to compute the fluxes?
 - In 2D single slip:
 - SSD (ρ) and GND (κ) densities?
 - $\rho = \rho_+ + \rho_-$
 - $\kappa = \rho_+ - \rho_-$
 - No multiplication, no annihilation

Continuum model of Groma

Equation of motion of individual dislocations



Coarse graining

Hierarchy of N -body densities



Assumption of short range correlations

Closed set of evolution equations for ρ and κ

I Groma, Phys Rev B, 1997

I Groma, M Zaiser, FF Csikor, Acta Mater, 2003

I Groma, M Zaiser, PD Ispánovity, PRB, 2016

Evolution equations w/o correlations

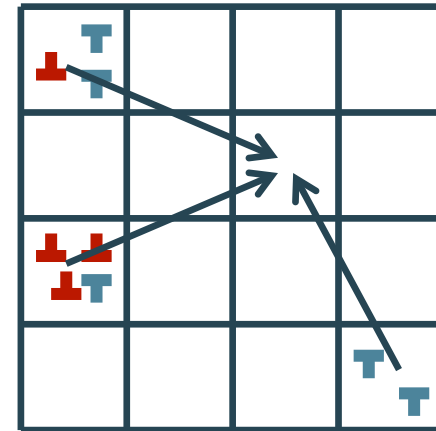
$$\partial_t \rho(\mathbf{r}, t) = -M_0 b \partial_x [\kappa \tau_{mf}]$$

$$\partial_t \kappa(\mathbf{r}, t) = -M_0 b \partial_x [\rho \tau_{mf}]$$

- M_0 : dislocation mobility
- b : Burgers vector
- τ_{mf} : mean-field stress
 - External load & long-range stresses generated by the GNDs

$$\tau_{mf}(\mathbf{r}, t) = \tau_{ext} + \int \kappa(\mathbf{r} - \mathbf{r}') \tau_{ind}(\mathbf{r}') d^2 r'$$

- Measurable quantity: the average local stress around a dislocation
- Plastic strain: $\partial_t \kappa(\mathbf{r}, t) = -(1/b) \partial_x \dot{\gamma}(\mathbf{r}, t)$



Evolution equations with correlations

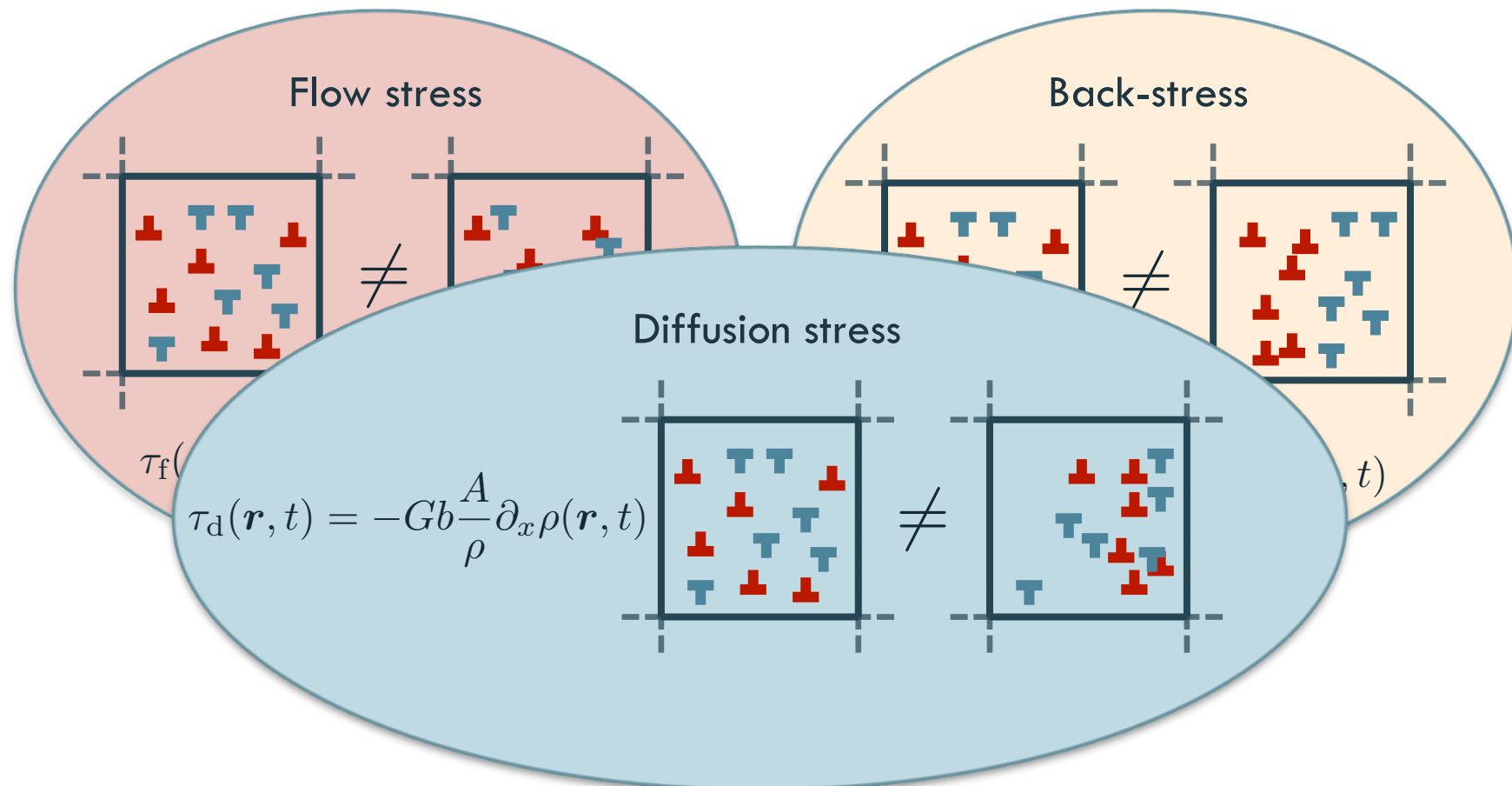
$$\partial_t \rho(\mathbf{r}, t) = -M_0 b \partial_x [\kappa \tau_{mf} - \kappa \tau_b + \rho \tau_d]$$

$$\partial_t \kappa(\mathbf{r}, t) = -M_0 b \partial_x \left[\rho \tau_{mf} - \rho \tau_b - \rho \left(1 - \frac{\kappa^2}{\rho^2} \right) \tau_f + \kappa \tau_d \right]$$

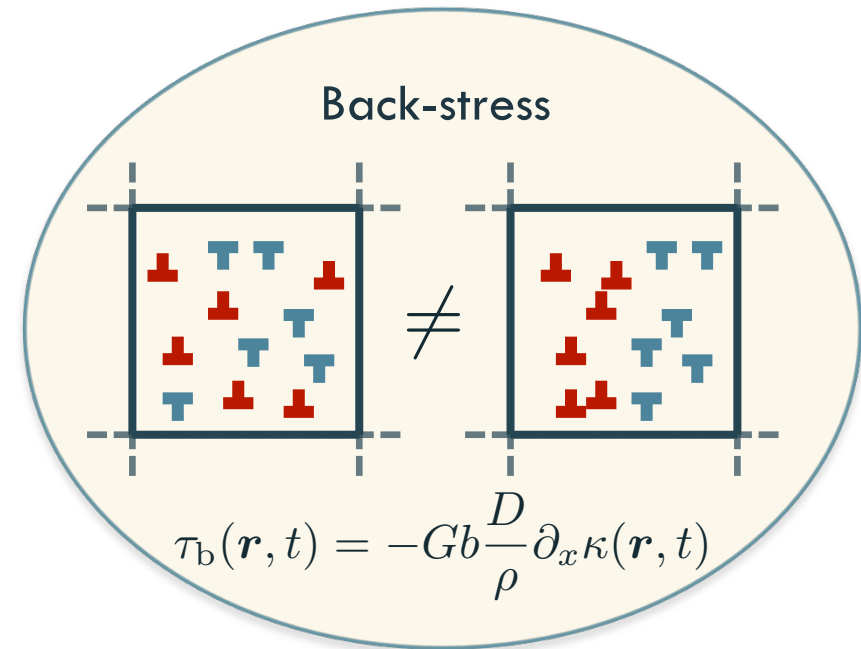
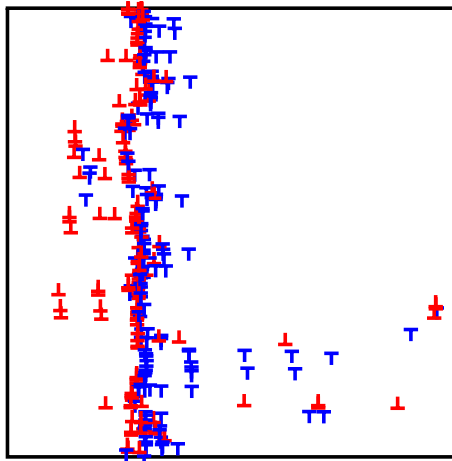
- Back-stress: $\tau_b(\mathbf{r}, t) = -Gb \frac{D}{\rho} \partial_x \kappa(\mathbf{r}, t)$
- Diffusion stress: $\tau_d(\mathbf{r}, t) = -Gb \frac{A}{\rho} \partial_x \rho(\mathbf{r}, t)$
- Flow stress: $\tau_f(\mathbf{r}, t) = \alpha \mu b \sqrt{\rho(\mathbf{r}, t)}$
- Dimensionless fitting parameters: D, A, α

Correlation induced stress terms

- The *representative volume element* (RVE) cannot resolve internal correlations



Strength of a dipolar wall



- In the middle of a dipolar wall: $\partial_x \rho = 0$ and $\partial_x \kappa < 0$
- The back-stress must be negative



$$D < 0$$

Implementation

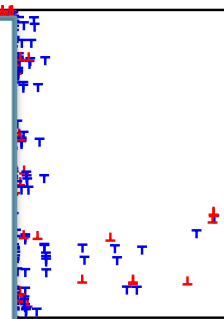
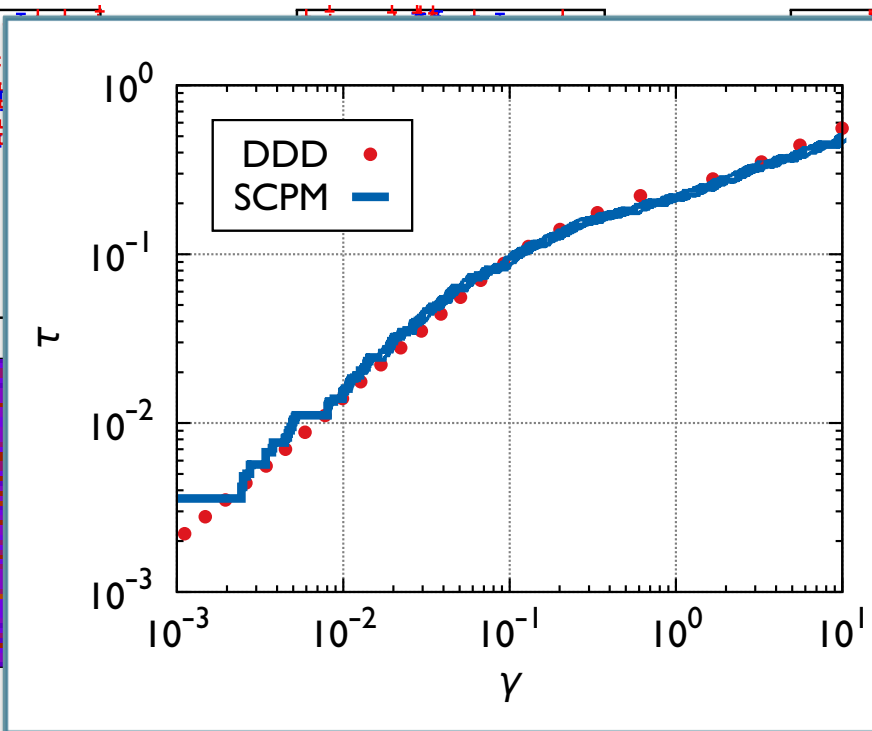
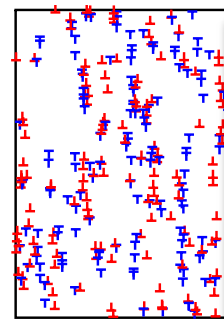
$$\partial_t \rho(\mathbf{r}, t) = -M_0 b \partial_x [\kappa \tau_{mf} + \kappa \tau_b + \rho \tau_d]$$

$$\partial_t \kappa(\mathbf{r}, t) = -M_0 b \partial_x \left[\rho \tau_{mf} + \rho \tau_b - \rho \left(1 - \frac{\kappa^2}{\rho^2} \right) \tau_f + \kappa \tau_d \right]$$

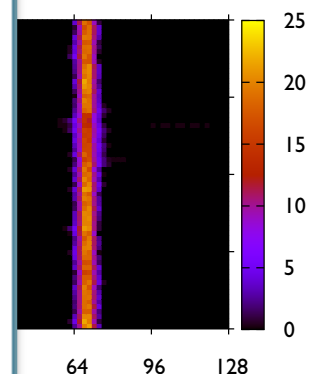
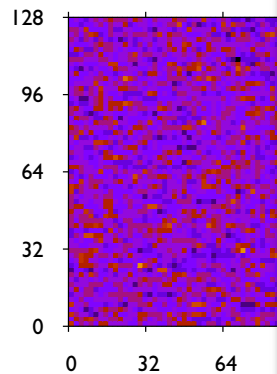
- CA implementation with extremal dynamics
- Dimensionless fitting parameters: D , A , α
- Flow stress is a stochastic variable
- No phenomenological assumptions

Evolution of density patterns

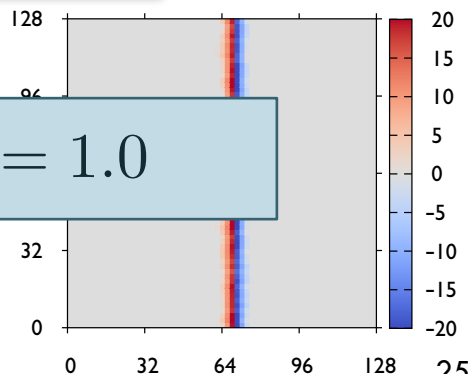
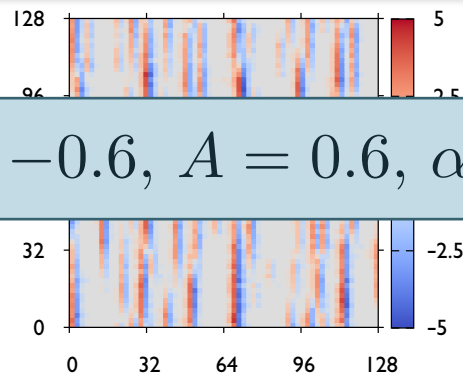
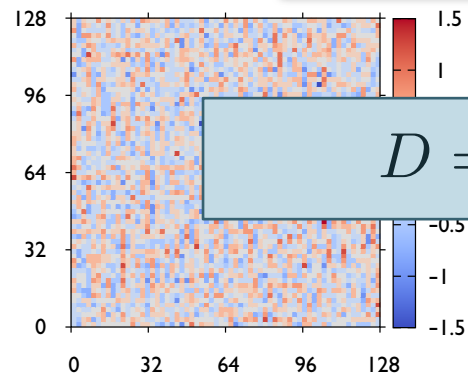
DDD configuration



Continuum
total density ρ



Continuum
GND density κ



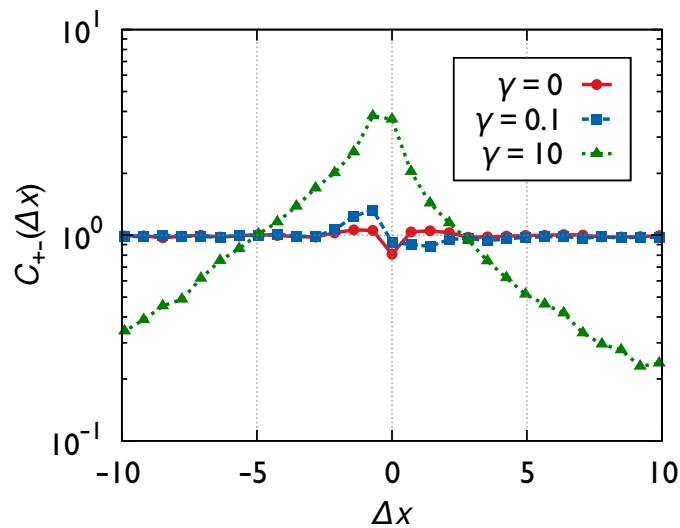
$$D = -0.6, A = 0.6, \alpha = 1.0$$

Characterization of pattern

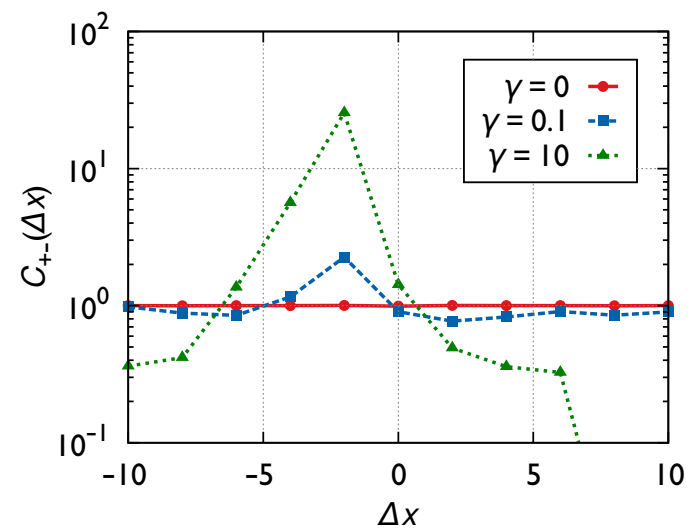
- Cross-correlation of + and – sign dislocations

$$C_{+-}(\Delta x, \Delta y) = \int \rho_+(x', y') \rho_-(x' + \Delta x, y' + \Delta y) dx' dy'$$

- $C_{+-}(\Delta x) := \langle C_{+-}(\Delta x, \Delta y) \rangle_{\Delta y}$:

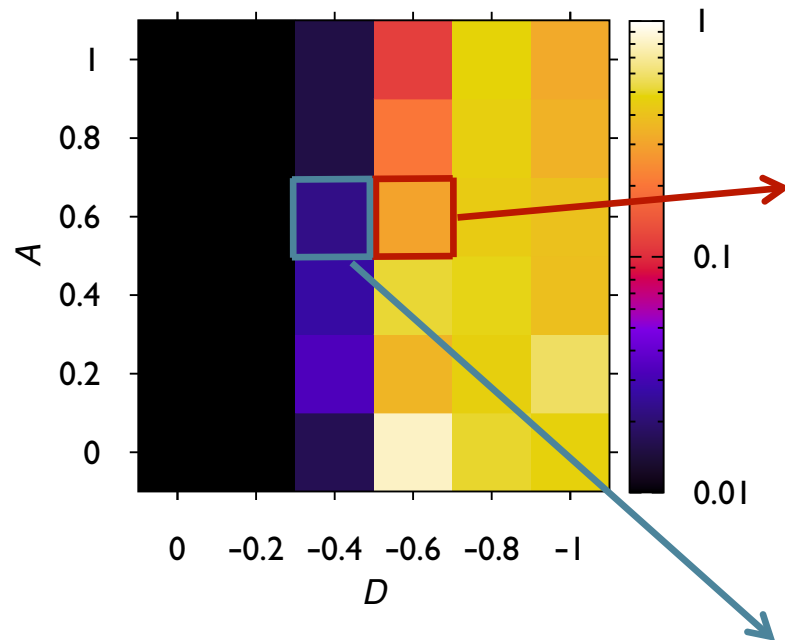


DDD

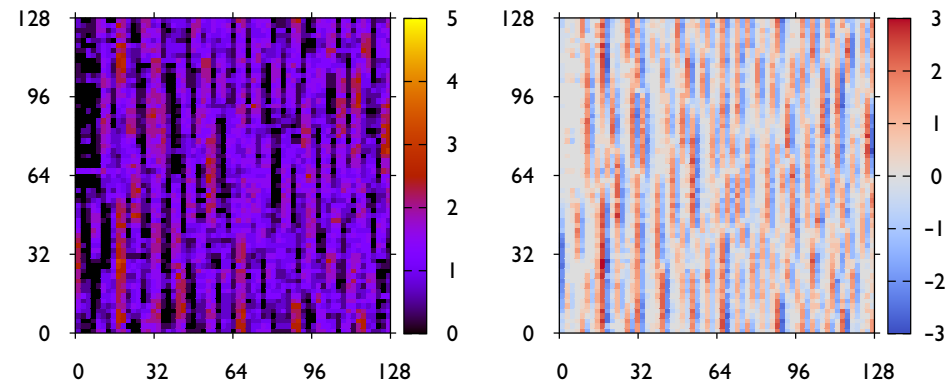


CDD

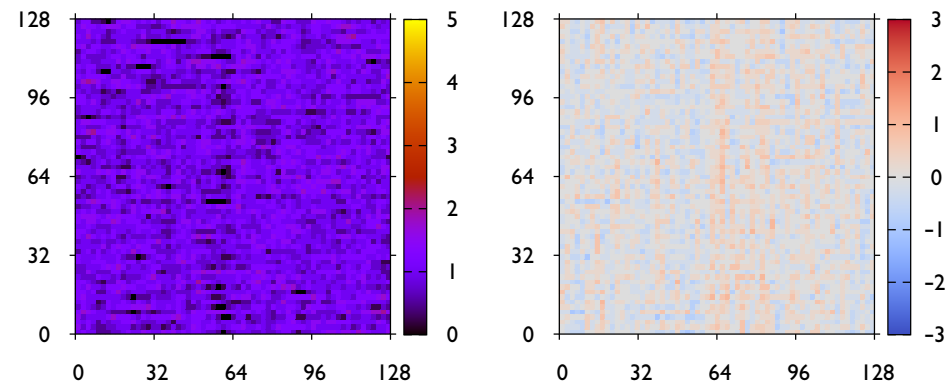
Effect of parameter D



- Order parameter: level of asymmetry in $C_{+-}(\Delta x)$

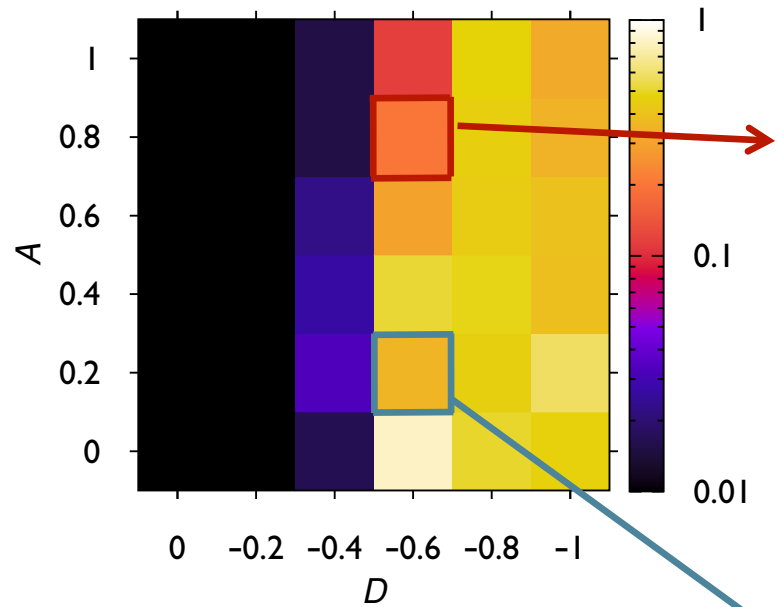


$$D = -0.6$$

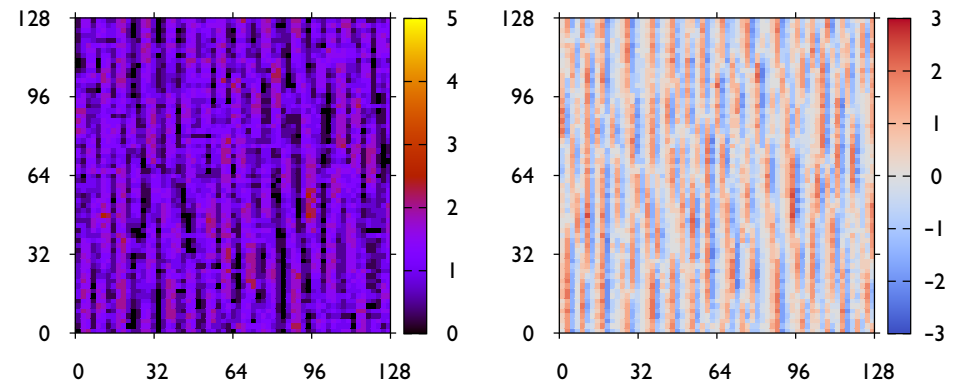


$$D = -0.4$$

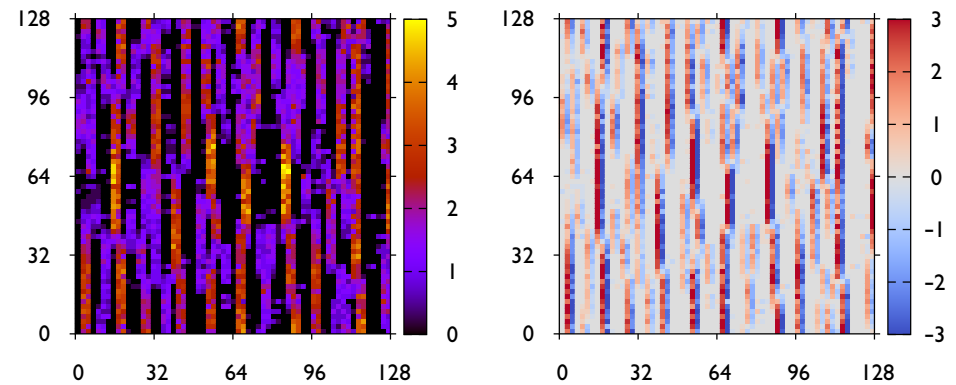
Effect of parameter A



- Order parameter: level of asymmetry in $C_{+-}(\Delta x)$



$A = 0.8$



$A = 0.2$

Summary

- 2D DDD is a simple toy model with very complex dynamics
 - Extended criticality
 - Anomalous system size dependence
- 2D continuum theory of dislocation dynamics
 - Derived analytically from the Eqs. of motion of discrete dislocations
 - There are no phenomenological assumptions, the gradient terms naturally emerge
 - Gradient terms are related to features of the microstructure: back-stress – dipolar walls
- The 2D continuum theory properly captures the patterning and the strain response of 2D DDD simulations
- Inclusion of back-stress is necessary for pattern formation